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砂兵器効果シミユレータ

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Ø

- 1. 兵器の模擬発射期間中に電磁波ピームを照射するよ う に構成された照射器と、入射した前記電磁波ビーム を検出するように構成された検出器とを備える兵器効 果シミュレータであつて、前配照射器は前配各発射と とに少くとも1つの電磁波パーストを発生するように 構成され、その電磁波パーストの持続時間は予め定め られ、かつ前配電磁波パーストは所定の周収数で変調 され、前記検出器は、前記所定の周波数に対して高調 放開係にある剧波数に同調され、かつ前記持続時間に 依存する通過帯域を有する周波数選択要素を含むこと を特徴とする兵器効果シミユレータ。
- 特許請求の範囲の第1項に記載のシミュレータであ つて、前配変調はパルス変調であることを特象とする シミュレータ。
- 3. 特許請求の範囲の第1項に記載のシミュレータであ つて、前配変異は持続波変绸であることを特象とする シミコレータ。
- 4. 特許請求の範囲の第1項に記載のシミュレータであ つて、前記周波数選択要素は前記所定の局波数に同議 させられることを特徴とするシミュレータ。
- 5. 特許請求の範囲の第1項に記載のシミュレータでも つて、前配通過帯域は前配持続時間の遊数の2倍にほ 仅等しいことを特徴とするシミュレータ。

- 停許請求の範囲の第1項に記載のシミユレータであ つて、前記検出器は1つの増艦器へ並列に結合される 複数の感光素子を有することを特徴とするシミユレー 丘 穏 効果シミユレータ

枝条的背景

本発明は兵器効果シミユレータに関するものである。

背景技術

それらの装置は、電磁放ビームを発生し、必要がある場合にはビームの向きを定めるための、服射器として一般に知られている装置と、標的に入射した電磁放を検出するための、検出器として知られている、別の装置とを含む。この検出器は標的自体にとりつけることもできれ

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時間は予め足められ、かつ前配電磁波パーストは所定の 周波数で変調され、前配検出器は、前配所定の周波数に 同調され、かつ前配持税時間に依存する通過帯域を有す る関波数速択要素を含む兵器効果シミュレータが得られる。

電磁波は、個々のパルスを別々に検出する(パルス変調の場合に)のではなくて、全体のパーストとその変調 (変調は、たとえば、パルス変調または特殊波変調にで きる)の検出により検出される。

周波数割択器の通過帯域は前配所定の持続時間の遊数の2倍にほぼ等しくできる。との持続時間を比較的長くすることにより(たとえば1ミリ秒)、通過帯域を非常に狭く(わずかに2KHェ)でき、それにより数個のホトセルを並列に結合できる程度まで、ノイズをかなり減少させることができる。

更に、与えられた B / N 比で放射せねばならないビーク電力は大幅に減少させられ、そのために、たとえばビーク出力が低く、平均出力が高い装置、たとえば二重へテロ構造レーザ D よび小型の発光ダイオードを用いることができる。

図面の簡単な説明

森村図面を参照して実施例を用い本発明の兵器効果シミュレータを説明する。ととで、第1図は射撃訓練兵と 標的兵を示す略図、第2図は照射器の一実施例のブロッ ば、傷的にとりつけられている反射器により反射されて きた 電磁波を受けるために無射器にとりつけることもで きる。

発明の開示

本発明の1つの面に従つて、兵器の模擬発射期間中に 電磁板ビームを照射するように構成された照射器と、入 射した前配電磁板ビームを検出するように構成された検 出器とを備える兵器効果シミュレータであつて、前記照 射器は前記各発射ごとに少くとも1つの電磁板パースト を発生するように構成され、その電磁板パーストの持続

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ク図、第3 図は照射器の別の実施例のブロック図、第4 図は検出器の回路図、第5、6 図はそれぞれバルス変調 と持続変変調を示すダイミング変形図である。

発明の実施のための最良の実施順様/産業上利用可能性

まず第 1 図を参照して、側線中の射撃兵 1 0 が 種的兵 1 4 に小鉄 1 2 のねらいをつけている。小鉄 1 2 には空包が 妥集されて かり、かつレーザ 照射器 1 6 がとりつけられている。 裸的兵 1 4 の 層部には 2 個の検出器 1 8 がとりつけられ、ベルト 2 2 には 4 個の検出器 2 0 がとりつけられる。全ての検出器 1 8 , 2 0 はベルト 2 2 にとりつけられている制御器 4 8 , 2 0 はベルト 2 2 にとりつけられている制御器 4 8 , 2 0 はベルト 2 2 にと

射撃兵10が小鉄12の引金を引くと空包が破裂して 音と光が生する。それと同時にレーザ照射器16が自動 的に動作させられて、電磁度ビームを小鉄12の無準の 向きに照射する。小鉄が緩的兵14に正確に照準されて おれば電磁度ビームが検出器18と20の少くとも一方 に入射して、信号が制御器かよび発煙器24へ送られる 。そうすると発煙器24から煙が出て緩的兵14に弾が 当つたことを示す。優的兵14も小鉄を持つているもの とすると、弾が当つた時にその小鉄の発射を禁止するよ りにその小鉄は制御器24へ結合される。

次に、無射器16と制御器24の構成と動作を第2~

6 図 を参照して詳しく説明する。

第 2 図に示されている無射器にかいては、小鉄1 2 の 発射 ごとに赤外欄のパルスのパーストが1 つだけ無射される。 しかし、希望によつては第3 図に示す回路を用いて、 各発材ごとにいくつかのパーストを無射させることができる。

次 化第 3 図を参照する。 発射センサ 3 0 は単安定回路 4 0 と 第 2 の 無安定回路 4 2 を 介して 無安定回路 3 4 へ 優続 される。 単安定回路 4 0 は ト リガされると持続時間 が 9 ミ リ杪の バルスを 無安定回路 4 2 へ 与える。 そうすると この 無安定回路 は 5 0 0 H ェ の 崗波数で動作する。

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検出器18,20(すなわち、感光素子50のいずれか)に入射した赤外線パルスのために、それに対応する電気パルスがコンデンサ54とトランス56を介して増幅器58ペルスがコンデンサ54とトランス56を介して増幅器58ペルスがコンデンサ54とトランス56を介して増幅された170 KHェのパルスの1ミリがパーストはフイルメ60により 戸破されてから比較器74ペ与えられる。この比較器74ペ与たられる。この比較器74ペ与た時に、発速器を作動させる。

第 5 図 • は典型的な赤外線パルスパーストのタイミング 放形図で、各 パルスパーストは、1 ミリ 秒期間中発生される、パルス間隔が 6 マイクロ秒で、パルス幅が 3 5 0 ナノ 秒の パルスで 構成される。 この 放 形に 等価 な 周波数 領域 を 第 5 図 b に 示す。 この 周波 数領域 は 0 日 ェ が中心である まローブと、1 7 0 K H ェの 整数倍が中心である 副ローブとを有する。各ローブは 2 K H ェの 周波 数 随 班 む 出

フイルタ60の作用は+170KH±と-170KH まを中心とするローブを選択することである。+170 KHェと-170KH±の符号の+とーは両方の信号の 位相が互いに逆であることを示すものである。フイルタ 60の過過管線2KHェはパルスパーストの周波数本ペクトラム中の2KHェ姫出に関連するもので、この地 は各パーストの持続時間1ミリ杪により決定される。し たがつて、フイルタ60の動作は、あるパーストが持続 されている間のそのパーストに含まれている全てのパル そのために無安定回路34は5周期だけ動作させられる。各周期の特殊時間は1ミリ秒で、周期と周期の間は1ミリ秒だけ隔でられる。無安定回路34の動作によりレーザ36は練り返えし周改数が170KHェの赤外線パルスパーストを5つ発射する。

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増幅器58の出力端子は3段帯取フイルタ60へ結合される。このフイルタの各段は増幅器62,64,64と、中心周波数が170KHIで、通過帯収幅が2KHIである証列共振帯収慮過LCフイルタ68,70,72でそれぞれ構成される。戸波された信号は比較器74へ与えられる。この比較器はダイオード検及一度調器76を介して発機器を制御する。

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170 KH s KF 同間している帯域フイルタ60を低域フイルタの代りに用いて、第5 図 b に示されている、0 H s を中心とする主ローブを検出することにより、周囲光の急変、またはこの装置の設置かよび設定中に受けるととができる。帯域フイルタ60は170 KH s 自体でなく、その高調改(たとえば340 KH s)に同調させることができる。更に、希望の帯域過過周故数に感光素子50の自己容量に組合わされて共協するととによりにチョーク52 のインダクタンスを演れてるととにより

結合トランス 5 6 より 前に周彼数選択 を行りことができる。

L C フイルタ 6 0 の代りにそれと同じ機能を果す他の回路装置、たとえば、希望の 2 K H ± 通過帯域を与えるように選択されたループ利得を有し、1 7 0 K H ± でクロックされる C C D 循環シフトレジスタを用いることができる。

以上説明した実施例はいろいろと変形して実施できる。たとえば、第3図の無安定回路の動作周波数を170 KHIから113KHIに変え、単安定回路40により 発生されるパルスの持続時間を短くして、小鉄12が発 射されるたびに113KHIの1ミリ秒パルスパースト を2個レーザ装置36が発生できるようにすることがで

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用い、「命中」(比較器74がトリガされる)と「外れ」(別の比較器はトリガされるが、比較器74はトリガされない)とを幾別できるようにすることもできる。

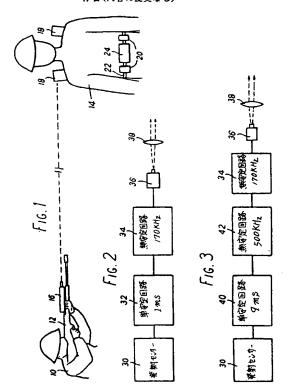
比較的低出力のレーザ装置36と、1つの低離音増盤 器58へ並列に接続される無パイアスの検出器18,20 を用いることにより、シミュレータのそれぞれの部品の電力消費量を大幅に減少することができるが、それらの部品は通常は電池を電源としているから、消費電力の低減は非常に重要である。

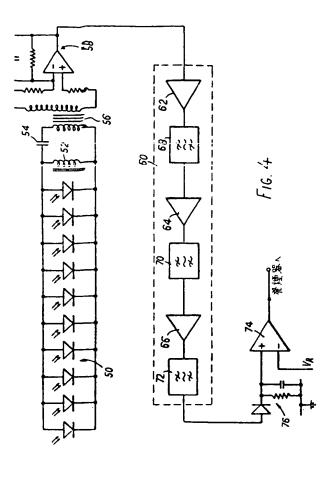
きる。第4図に示されている検出器の回路、(1)帝城 フイルタ60の各段をレーサのパルス繰り起えし周放数 の第 4 高調波すなわち 4 5 2 K H z に同調させ、(👂) それに対応して増幅器58の上限運断局度数を高くし、 (■) 4 7 0 K H ± 化同調されている別の帯域フイルタ を増幅器58の出力端子へ接続することにより変えた。 それらのフィルタはともにセラミック・フィルタ業子を 用いた。前配別のフイルタの出力は、第4回に示されて いるダイオード検徴ー復調器でもと同じ検皮ー復調器と 増幅度が3の増幅器を介して、比較器74の反転入力増 子へ電圧V。として加えられる。この比較器74の出力 は二重パルス検出器、すなわち、所定の時間(たとえば 1.5ミリ秒)以内での2個の連続パルスの発生を検出 する検出器へ与えられる。との実施例の動作においては 、広帯域ノイズすなわち番単性のノイズが2つのダイオ ード検放ー復興器から経済等しい出力を生じさせるから 、それらのノイズによつて比較器74はトリガされると とはなく、したがつて二重パルス検出器の個トリガは防 止される。実際には、増幅度が3の増幅器により、ダイ オード検波ー復調器76の出力が他のダイオード検波復 調器の出力より3倍以上大きい時だけ、比較器14をト

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希望によつては、比較器74に類似するが、ダイオード検放-復調器76からのより小さな振幅(すなわち低い相対振幅)のベルスによりトリガされる別の比較器を

浄書(内容に変更なし)





正 書(方式) 手 統 補

3月16日

特許庁長官

1. 事件の表示

昭和 年 特 計 類 弟 P C T / G B 80 / 000 9 2 / 田和

2. 発明の名称

兵器効果シミユレータ

3. 補正をする者 事件との関係 特許出願人

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弁 理 士

5. 補正命令の日付

昭和 5 6 年 2 月 20 日 (発送日 開報 56 年 2 月 24 日)

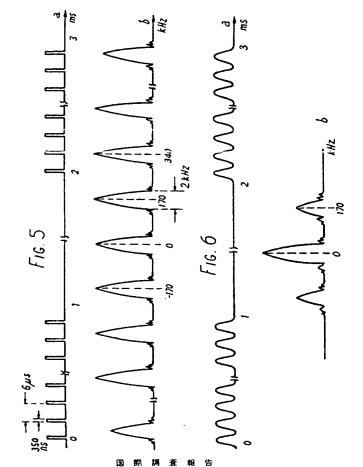
6. 補正により

7. 補正の対象

図面の翻訳文

8. 補正の内容

図面の勧択文の浄書(内容に変更なし)



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	US,	A, 4054290, published see figure 1; column a A.J. Villa	October 18, 1977 2, lines 21-40,	1,4
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	us,	A, 3918714, published see figures 1,2; colu column 3, lines 14-18	mn 2, lines 29-61;	1,4
	us,	A, 3257741, published see figure 1; from co to column 3, line 23; 40-41, S.H. Cameron e	lumn 1, line 48, column 4, lines	1', 6
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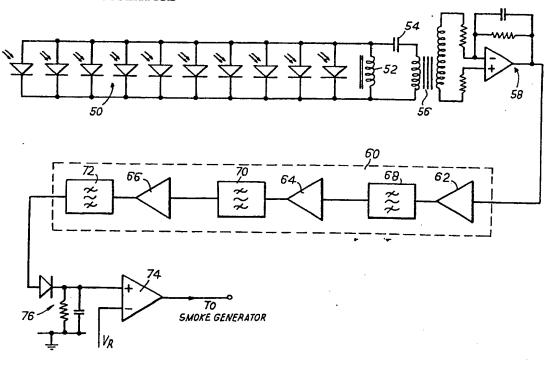
GB

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- (72) Inventors; and
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Published

With international search report

(54) Title: WEAPON EFFECT SIMULATORS



(57) Abstract

In a weapon effect simulator a low peak power laser projector (16) emits 1 milli-second bursts of radiation, each burst having either pulse or c.w. modulation at 170 kHz. A detector (18, 20, 24) for sensing the radiation has several photo-cells (50) connected in parallel to a single amplifier (58), and includes a bandpass filter (60) tuned to 170 kHz (chosen in harmonic relationship to the modulation frequency) and having a passband of 2kHz (inversely related to the duration of each radiation burst).

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WEAPON EFFECT SIMULATORS

TECHNICAL FIELD

This invention relates to weapon effect simulators.

BACKGROUND ART

It is known to use a beam of electromagnetic radiation (typically from a laser) during simulated operation of a weapon for training purposes. In one type of system (UK Patent Specifications Nos. 1 228 143, 1 228 144, 1 439 612 and 1 451 192), the beam of radiation is pointed in the same direction as the weapon (for example, a gun) at the time of 'firing' the ammunition (a shell or bullet) with adjustment for such factors as aim-off if appropriate. In another type (UK Patent Specifications Nos. 1 300 941 and 1 300 942) the beam is pointed to intersect continuously the path that the ammunition (for example, a missile) would follow in a live firing. In either case, the result is that the beam of radiation is directed at the point in space occupied by the ammunition when it reaches the vicinity of the target.

Such systems basically involve a device, commonly known as a projector, for generating, and if necessary orienting, the beam of radiation, and another device, known as a detector, for detecting incidence of the radiation on the target. The detector may be mounted on the target itself, or it may be associated with the projector, the radiation being reflected from the target by a retro-reflector mounted thereon.

In known systems, the projector has been arranged to generate radiation in the form of pulses of very short duration and relatively high peak power. Consequently, the detector (a photo-cell coupled to an amplifier) has been designed essentially to detect each pulse of radiation as an individual, discrete entity. Because of the abrupt nature of the pulses, the bandwidth of the detector amplifier has to



be relatively large to ensure reliable detection of a pulse, which in turn limits to one the number of photo-cells which can be connected to an amplifier if an acceptable signal-to-noise ratio is to be maintained. In practice, a target needs to be fitted with at least four photo-cells to ensure detection of radiation from any direction around the target, and each of these photo-cells requires its own sensitive, stable, wide-bandwidth (and therefore expensive) amplifier.

DISCLOSURE OF INVENTION

According to one aspect of this invention there is provided a weapon effect simulator having a projector arranged to project a beam of electromagnetic radiation during simulated firing of a weapon and a detector arranged to detect incidence of said radiation thereupon, wherein:

said projector is arranged to generate at least one burst of radiation for each said firing, said burst being of predetermined duration and being modulated at a predetermined frequency;

and

said detector includes frequency-selective means tuned to a frequency harmonically related to said predetermined frequency and having a pass band dependent upon said predetermined duration.

The radiation is detected by detection of the overall burst and its modulation (which can, for example, be pulse modulation or continuous-wave modulation), rather than by separate detection of individual pulses (in the case of pulse modulation). The frequency-selective means is conveniently tuned to said predetermined frequency.

The pass band of the frequency-selective means may be substantially equal to twice the reciprocal of said predetermined duration. By making this duration relatively long (for example, one millisecond), the pass band can be made very narrow (only 2 kHz), thereby diminishing noise considerably, to the extent that several photo-cells can be coupled in parallel. Furthermore the peak power that must be



radiated for a given signal-to-noise ratio is substantially reduced, permitting the use, for example, of low peak power, higher mean power devices such as double heterostructure lasers and small source light emitting diodes.

BRIEF DESCRIPTION OF DRAWINGS.

A weapon effect simulator in accordance with this invention will now be described, by way of example, with reference to the accompanying drawings, in which:-

Figure 1 depicts an attacking soldier and a target soldier;
Figure 2 is a block schematic diagram of one form of projector;

Figure 3 is a block schematic diagram of another form of projector;

Figure 4 is a circuit diagram of a detector; and

Figures 5 and 6 are waveform and spectral diagrams illustrating pulse modulation and continuous-wave modulation respectively.

BEST MODE FOR CARRYING OUT THE INVENTION/INDUSTRIAL APPLICABILITY

Referring to Figure 1, an attacking soldier 10 under training is aiming a rifle 12 at a target soldier 14. The rifle 12 is loaded with blank ammunition and carries a laser projector 16. The target soldier 14 has two detectors 18 on his shoulders and four more detectors 20 on a belt 22 about his waist. All the detectors 18 and 20 are connected to a control unit and smoke generator 24 also carried on the belt 22.

When the soldier 10 pulls the trigger of the rifle 12, the blank ammunition is fired, giving appropriate aural and visual effects. At the same time, the laser projector 16 is automatically operated to project a beam of electromagnetic radiation along the direction of aim of the rifle 12. If the rifle 12 has been accurately aimed at the soldier 14, the radiation will strike the detectors 18 and/or 20, causing a signal to be sent to the control unit 24 which thereupon releases smoke to indicate that the target soldier 14 has been 'hit'. If the target soldier 14 has a rifle, this can be coupled to the control unit 24 to be inhibited



from 'firing' in the eyent of a 'hit'.

The design and operation of the projector 16 and the control unit 24 will now be described in more detail with reference to Figures 2 to 6.

Referring to Figure 2, the firing of the rifle 12 is detected by a firing sensor 30, which may be, for example, a microphone and amplifier to detect the sound of the rifle 12 being fired, or a pressure-responsive switch operated by the back pressure in the rifle barrel when the blank ammunition is fired. The sensor 30 triggers a monostable circuit 32 which supplies a pulse of 1 millisecond duration to enable an astable circuit 34. This astable circuit 34 supplies pulses at a repetition frequency of 170 kHz to a gallium arsenide double-heterostructure laser device 36, to generate pulses of infra-red radiation at a rate of 170 kHz for 1 millisecond. A lens in front of the laser device 36 focusses the radiation into a beam.

In the projector illustrated in Figure 2, only a single burst of pulses of radiation is emitted each time the rifle 12 is fired. However, if desired, several bursts may be emitted for each firing, using the circuit shown in Figure 3.

Referring to Figure 3, the firing sensor 30 is coupled to the astable circuit 34 via a monostable circuit 40 and a second astable circuit 42. The monostable circuit 40, when triggered, supplies a pulse having a duration of 9 milliseconds, thereby enabling the astable circuit 42 which runs at a frequency of 500 Hz. Thus the astable circuit 34 is in turn enabled for five periods each 1 millisecond in duration and spaced 1 millisecond apart, and the laser device 36 emits five corresponding bursts of 170 kHz pulses of infra-red radiation.

Referring now to Figure 4, the detectors 18, 20 are



represented by ten unbiassed photo-sensitive silicon cells 50 connected in parallel with each other and with a choke 52. The choke 52 provides a d.c. leakage path for charge induced in the cells 50 by ambient light, thereby preventing such charges from accumulating and saturating the cells 50. High-frequency signals, which are not affected by the choke 52, are coupled by a capacitor 54 to a primary winding of a coupling transformer 56. The turns ratio of this transformer 56 is selected for optimum signal-to-noise ratio, and the secondary winding of the transformer feeds a low-noise amplifier 58 of conventional design, having a low-value feedback capacitor to limit its high-frequency response.

The output of the amplifier 58 is coupled to a three-stage bandpass filter 60, each stage of which comprises an amplifier 62, 64, 66 and an associated parallel-resonant bandpass LC filter 68, 70, 72 tuned to 170 kHz and having a passband of 2 kHz. The filtered signal is then supplied to a comparator 74, which controls the smoke generator, via a diode detector-demodulator 76.

In use, pulses of infra-red radiation incident upon any of the detectors 18, 20 (that is, on any of the photo-cells 50) cause corresponding electrical pulses to be supplied via the capacitor 54 and the transformer 56 to the amplifier 58. After amplification, the 1 millisecond bursts of 170 kHz pulses are selectively passed by the filter 60 to the comparator 74 which actuates the smoke generator if the amplitude of the filtered signal exceeds a threshold voltage $V_{\rm R}$.

Figure 5 (a) shows the waveform of typical bursts of infra-red radiation, each comprising pulses 350 nanoseconds long repeated at intervals of 6 microseconds for a period of 1 millisecond. The frequency-domain equivalent of this waveform is shown in Figure 5 (b), and comprises a main lobe centred on 0 Hz and additional lobes centred on integral multiples of 170 kHz, each lobe embracing a frequency range of 2 kHz.



The effect of the filter 60 is to select the lobes centred on + 170 kHz and - 170 kHz (where the negative sign indicates a signal in anti-phase to one having a positive sign). The 2 kHz passband of the filter 60 is related to the 2 kHz range of the lobes in the frequency spectrum of the pulse bursts, and this range is in turn determined (on an inverse basis) by the 1 millisecond duration of each burst. The operation of the filter can thus be considered as being the integration of all the pulses of a burst for the duration of the burst, so the energy associated with each individual pulse is aggregated with that of all the other pulses in the burst. Consequently, a laser device which is capable of relatively high mean power but relatively low peak power, such as the (relatively cheap) double heterostructure device mentioned previously, can be used in the projector 16. This is turn confers advantages in terms of stability of operation of the projector with change in temperature, and permits the use of small, low-voltage drive transistors with the laser device. The relatively narrow (2 kHz) bandwidth of the filter 60 also significantly limits the proportion of the noise signal from the photo-cells 50 which can reach the comparator 74, thereby facilitating the use of a low peak power laser device and permitting the parallel connection of several photo-cells 50 to a single amplifier 58 as shown in Figure 4.

Using the bandpass filter 60 tuned to 170 kHz instead of a low pass filter (to detect the main lobe centred on 0 Hz - Figure 5b), avoids spurious output signals arising either from sudden changes in ambient light or from artificial light sources to which the apparatus may be exposed during fitting and setting up. The bandpass filter 60 could be tuned to a harmonic of the pulse repetition frequency (such as 340 kHz) rather than to the repetition frequency of 170 kHz itself. Furthermore, the frequency selection could be performed before the coupling transformer 56, by selecting the inductance of the choke 52 to resonate with the combined self-capacitance of the photo-cells 50 at the desired bandpass frequency.



Instead of pulse modulation of the radiation emitted by the projector 16, it is also possible to use continuous-wave modulation, as illustrated in Figure 6 (a). In this case, the astable circuit 34 of Figures 2 and 3 would be replaced by a suitable sine-wave oscillator. Figure 6 (b) shows the frequency spectrum of this type of modulation, for which the bandpass filter 60 would be tuned to the modulation frequency (170 kHz) of the 1-millisecond bursts of radiation. With c.w. modulation, for which a striped-geometry type of laser or small source light emitting diode is particularly suitable, rather more of the modulation power (up to half) can be extracted by the filter 60 than is the case with pulse modulation.

The LC filter 60 could be replaced by other circuitry having the same function, such as a CCD recirculating shift register clocked at 170 kHz and having a loop gain chosen to provide the desired 2 kHz passband.

Various other modifications can be made to the described embodiment of the invention. For example, in another embodiment of the invention, the operating frequency of the astable circuit of Figure 3 was changed from 170 kHz to 113 kHz, and the duration of the pulse produced by the monostable circuit 40 was reduced so that the laser device 36 produced two 1 millisecond bursts of 113 kHz pulses of infra-red radiation for each firing of the rifle 12. The detector circuitry of Figure 4 was also modified, by (i) tuning each stage of the bandpass filter 60 to the fourth harmonic of the laser p.r.f, that is to 452 kHz, (ii) correspondingly increasing the upper cut off frequency of the amplifier 58, and (iii) connecting a further bandpass filter, tuned to 470 kHz, to the output of the amplifier 58: both bandpass filters used ceramic filter elements. The output of this further filter was applied, via a diode detector-demodulator identical to that shown at 76 in Figure 4 and a x3 amplifier, to the inverting input of the comparator 74 (i.e. as the voltage $V_{\rm p}$). The output of the comparator 74 was then connected to a double-pulse detector, ie a detector which



detects the occurrence of two consecutive pulses within a predetermined time period, eg l½ milliseconds. In operation of this embodiment, wide-band or impulsive noise tended to produce substantially equal outputs from both the diode detector-demodulators, so the comparator 74 was not triggered by such noise and spurious triggering of the double-pulse detector was prevented. In fact, the x3 amplifier ensures that the comparator 74 can be triggered only when the signal appearing at the output of the diode detector-demodulator 76 exceeds that at the output of the other diode detector-demodulator by more than a factor of three.

If desired, a further comparator similar to the comparator 74, but triggered by pulses of lower amplitude (or lower relative amplitude) from the diode detector-demodulator 76, can be provided, in order to permit a distinction to be made between a "hit" (comparator 74 triggered) and a "near miss" (further comparator triggered, but comparator 74 not triggered).

The use of the relatively low-powered laser device 36, and the use of the unbiassed detectors 18, 20 connected in parallel to the single low-noise amplifier 58, each help to significantly reduce the power consumption of their respective parts of the simulator, which, since these parts are normally battery-powered, is very important.



CLAIMS

1. A weapon effect simulator having a projector arranged to project a beam of electromagnetic radiation during simulated firing of a weapon and a detector arranged to detect incidence of said radiation thereupon, characterised in that:

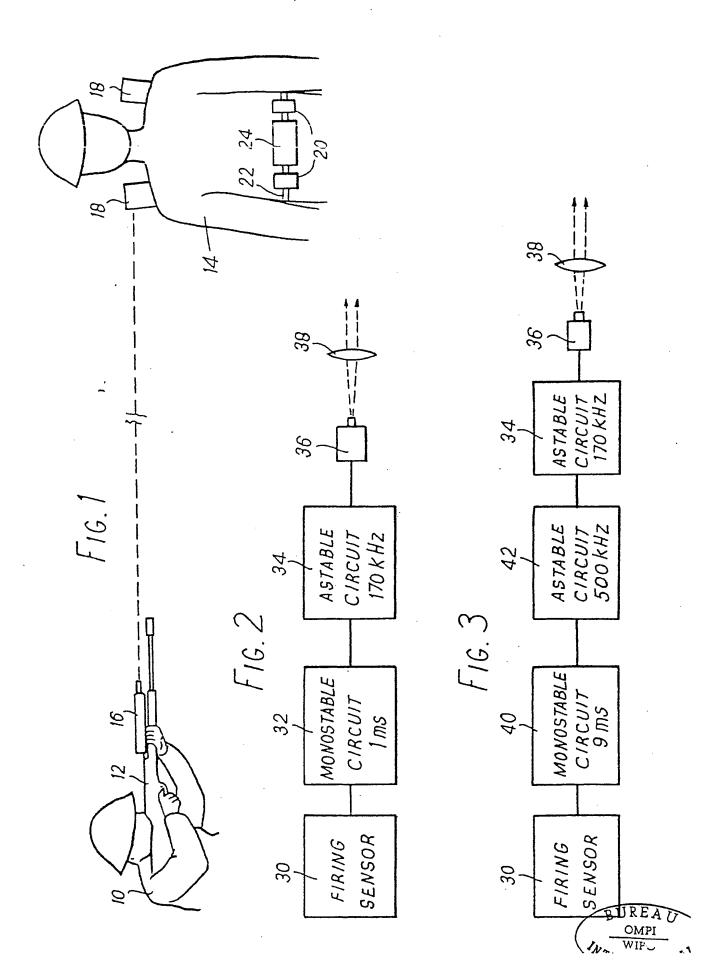
said projector is arranged to generate at least one burst of radiation for each said firing, said burst being of predetermined duration and being modulated at a predetermined frequency;

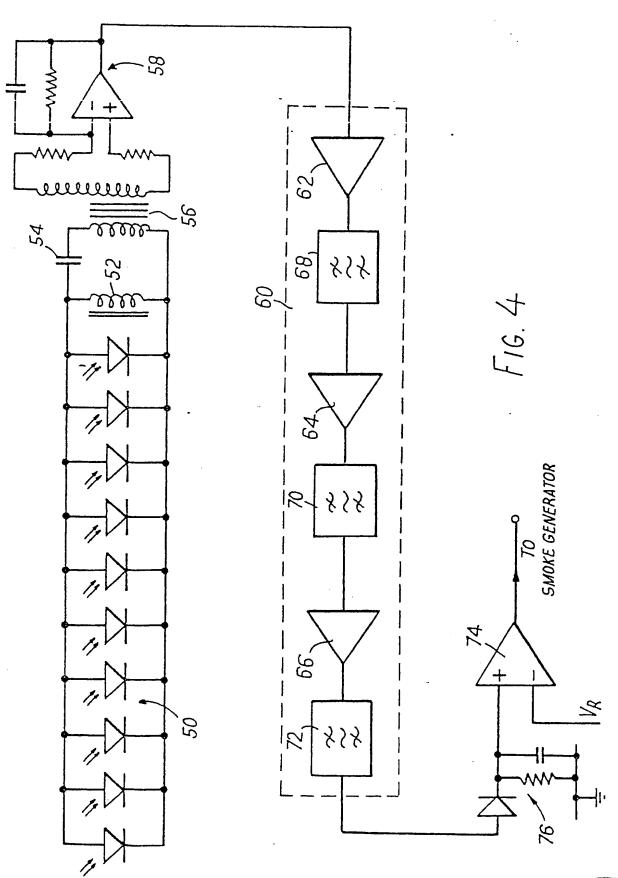
and in that

said detector includes frequency-selective means tuned to a frequency harmonically related to said predetermined frequency and having a pass band dependent upon said predetermined duration.

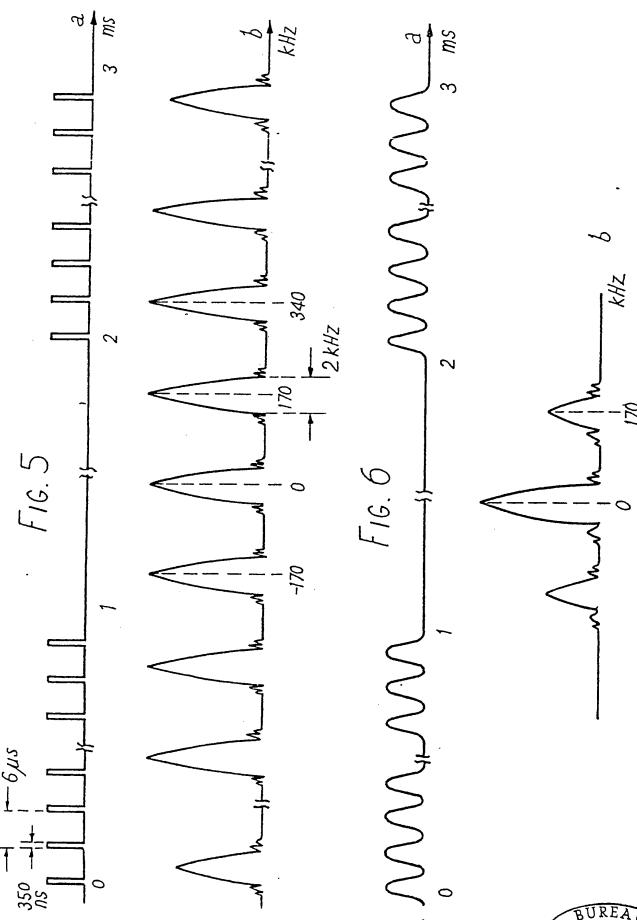
- 2. A simulator according to claim 1, wherein said modulation is pulse modulation.
- 3. A simulator according to claim 1, wherein said modulation is continuous-wave modulation.
- 4. A simulator according to claim 1, wherein said frequency-selective means is tuned to said predetermined frequency.
- 5. A simulator according to claim 1, wherein said pass band is substantially equal to twice the reciprocal of said predetermined duration.
- 6. A simulator according to claim 1,
 wherein said detector has a plurality of light-sensitive
 cells coupled in parallel to a single amplifier.







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IV. CERTIFICATION "X" document of particular relevance				
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11				
	SERVATIONS WHERE CERTAIN CLAIMS WERE FOUND UNSEARCHABLE 10			
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2. As only some of the required additional search fees were timely paid by the applicant, this international search report covers only those claims of the international application for which fees were paid, specifically claims:				
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